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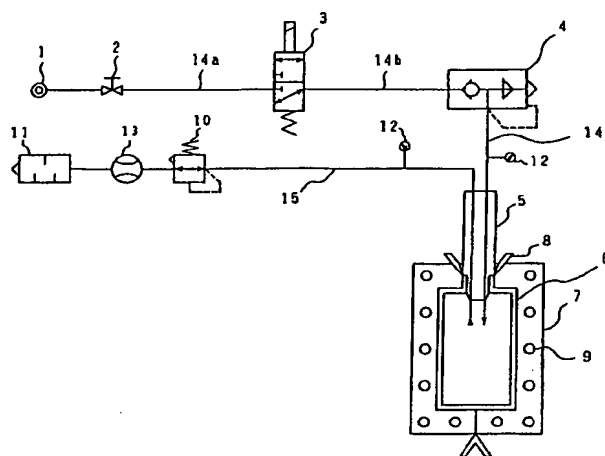
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(54) BLOW MOLDING METHOD

(57) In a blow molding process in which a gas is blown into a parison within a mold (7) to inflate the parison so that the parison is intimately contacted with a mold shaping portion to form a hollow molded product (6), and the gas within the hollow molded product (6) is discharged for the purpose of cooling, the blow molding process being characterized in that an internal gas pressure of the hollow molded product (6) is set to 5 to 8 kgf/cm² (G) and the gas satisfying the expression $F \geq 10 \times W$ [where F: gas flow rate (Nl/min) and W: hollow molded product weight (g)] is discharged while blowing.

Fig. 1**EP 0 919 355 A1**

Description

Technical Field

- 5 [0001] This invention relates to a blow molding process of a plastic product, and more particular to a blow molding process in which a cooling is performed from the insides of a mold and a hollow molded product.

Background Art

- 10 [0002] In a blow molding, after a sleeve-like molten resin called parison extruded from an extruder is sandwiched between mold halves of a split mold, air is blown into the parison to inflate it so that a configuration of the mold cavity is applied to the inflated parison, and then the parison is cooled and hardened within the mold to obtain a desired hollow molded product.

- [0003] In the blow molding, although the outside of a hollow molded product such as a bottle, or the like is cooled because it contacts the mold through which a cold water circulates, the inside of the hollow molded product is not cooled because the inside is in a heat insulated state. In case the inside of the hollow molded product is not cooled as just discussed, the pressure inside the hollow molded product becomes an original pressure of air to be introduced and the hollow molded product can be cooled by being intimately contacted with the mold. However, since only the cooling effect is obtained from the mold, cooling efficiency is bad.

- 20 [0004] A cooling method is disclosed in Japanese Patent Laid-Open Publication (Tokkai) No.3(1991)-13313, in which the pressure inside the hollow molded product is, in order to reduce the time for cooling, maintained at a prescribed pressure level and then air is discharged while blowing air into the interior of the hollow molded product, so that the hollow molded product is cooled also from the inside.

- [0005] Japanese Patent Laid-Open Publication (Tokkai) No.3(1991)-222714 discloses a device in which an air blowing tube for introducing air, and a discharge tube for discharging air within a hollow molded product are, in order to enhance the inside cooling efficiency, located away from each other so that the air flows the entire hollow molded product. Further, Japanese Patent Laid-Open Publication (Tokkai) No.5(1993)-104615 discloses a device in which an air blowing port is rotated under air pressure so that the air is blown to the entire hollow molded product.

- 25 [0006] However, in case air is discharged while blowing air into the hollow molded product, the pressure within the hollow molded product becomes lower than the original pressure of the air. For this reason, the force for urging the parison against the mold becomes small compared with a case where no inside cooling is performed, and the cooling effect from the mold is lowered than in the case where no inside cooling is performed.

- [0007] That is, in the conventional inside cooling process, the cooling effect from the inside is available but on the other hand, the cooling effect from the mold is lowered. As a consequence, it is unable to obtain a sufficient cooling effect.

Disclosure of Invention

- 40 [0008] It is, therefore, an object of the present invention to provide a blow molding process in which the cooling effect from a mold and the cooling effect from the inside of a hollow molded product are effectively obtained and therefore, the hollow molded product can be blow molded under a large cooling effect.

- [0009] As a result of a hard study for achieving the above object, the present applicant found out the fact that by setting the inside gas pressure of the hollow molded product within a certain range, the cooling effect from both the inside and outside of the hollow molded product can be efficiently and sufficiently exhibited without lowering the cooling effect from the mold and by cooling the inside with a prescribed quantity or more of cooling gas such as air, or the like.

- 45 [0010] The present invention has been made based on the above finding. According to the present invention, there is provided in a blow molding process in which a gas is blown into a parison within a mold to inflate the parison so that the parison is intimately contacted with a mold shaping portion to form a hollow molded product, and the gas within the hollow molded product is discharged for the purpose of cooling, the blow molding process being characterized in that an internal gas pressure of the hollow molded product is set to 5 to 8 kgf/cm² (G) and the gas satisfying the expression $F \geq 10 \times W$ [where F: gas flow rate (N l/min) and W: hollow molded product weight (g)] is discharged while blowing.

- 50 [0011] The inside gas pressure of the hollow molded product and the flow rate of the gas are defined within the above-mentioned ranges based on the following test result.

- [0012] In Fig. 2, the temperature for removing the hollow molded product is measured without performing an inside cooling but by changing the original pressure (blowing pressure) of air. The molding conditions are as follows.

Bottle capacity	200 ml
Bottle weight	20 g

Resin	high density polyethylene (HDPE)
Resin thickness	body portion 0.5 to 1.5 mm bottom portion 1 to 3 mm
Blowing time	6 sec.
5 Discharging time	1 sec.
Blowing air temperature	20 °C
Mold cooling water temperature	17 °C

[0013] As shown in Fig. 2, the lower the pressure within the bottle is, the more the force for urging the parison against the mold is decreased. For this reason, the effective contact area with the mold is reduced. Further, since the molded product is contracted with the progress of cooling, a gap between the molded product and the mold is enlarged. As seen, when the original pressure of air is decreased, the cooling effect from the mold tends to be decreased and the temperature for removing is increased.

[0014] The present applicant found out from this result the fact that if the original pressure (blowing pressure) of air is set to 5 to 8 kgf/cm² (G) or more, the cooling effect from the mold becomes constant. The reason seems to be as follows. If the force for urging the resin against the mold is 5 to 8 kgf/cm² (G) or more, the effective contact area of a molten resin with the mold is unchanged and the molded product is not easily removed from the mold even if the molded product is contracted. As a consequence, the cooling effect from the mold becomes constant.

[0015] In Figs. 3 and 4, in case the inside cooling is performed, when the original pressure of air is 5 kgf/cm² (G) or 10 kgf/cm² (G) and the removing temperature is measured by varying the pressure within the bottle. In Figs. 3 and 4, in case the pressure within the bottle is 5 kgf/cm² (G) when the original pressure of air is 5 kgf/cm² (G), it indicates a state that no inside cooling is performed. In case the pressure within the bottle is 10 kgf/cm² (G) when the air original pressure is 10 kgf/cm² (G), it indicates a state that no inside cooling is performed.

[0016] First, let's review the case where the original pressure of the bottle is 5 kgf/cm² (G).

[0017] Up to 2 to 5 kgf/cm² (G) of the pressure within the bottle, the removing temperature is decreased because the cooling effect from the inside overcomes the decrease of the cooling effect from the mold. For example, in case the pressure within the bottle is set to 4 kgf/cm² (G) and the flow rate of the air is set to 100 Nl/min, the removing temperature is lowered by 10 to 15 °C, compared with the case where no inside cooling is performed.

[0018] If the pressure within the bottle is lowered to 2kgf/cm² (G) or less, an apparent removing temperature is not changed in spite of the fact that air of the flow rate of 200 to 230 Nl/min flows because the cooling effect from the inside is offset by the decrease of the cooling effect from the mold. In this case, the removing temperature is lowered by 15 °C compared with the case where no inside cooling is performed.

[0019] However, in case the air was flowed at a flow rate of 300 Nl/min by increasing the original pressure of air to 10 kgf/cm² (G) while maintaining the pressure within the bottle at the level of 6 kgf/cm² (G), the removing temperature could be lowered by 20 °C to 30 °C compared with the case where no inside cooling was performed.

[0020] It should be noted, however, that in case the pressure within the bottle is maintained at the level of 4 kgf/cm² (G), the removing temperature is not changed even if air of the flow rate of 360 Nl/min is flowed because the cooling effect from the mold is lowered, thus resulting in wasteful use of air.

[0021] That is, by blowing a large amount of air into the bottle and discharging the air therefrom in the state that the pressure within the mold is set such that the cooling effect from the mold becomes maximum, a large cooling effect can be obtained by using air efficiently.

[0022] Next, the flow rate of air necessary for cooling the inside is reviewed.

[0023] Fig. 5 shows a relation between the air flow rate and the temperature difference between the blowing air and the discharging air of Figs. 3 and 4.

[0024] The heat transmitting speed from the resin to the air in case the inside cooling by air is performed, is determined by a heat transfer coefficient of the air from the resin and the difference between the surface temperature of the resin and the air temperature.

[0025] Accordingly, if the air flow rate is increased, the boundary film in the nearby area of the resin surface is reduced in thickness and the heat transmitting amount from the resin to the air is increased to greatly increase the degree of the increase of air temperature. However, since the difference between the resin surface temperature and the air temperature is also decreased, the degree of increase of the air temperature is generally constant at 25 °C, i.e., the discharged air temperature becomes generally constant at 45 °C.

[0026] A specific decrease of the removing temperature due to specific seconds for performing the inside cooling depends on the thickness of the hollow molded product, the capacity of the hollow molded product, etc. With respect to a bottle having a thickness up to 0.5 to 3 mm, the removing temperature in case the inside cooling is performed for about 7 seconds is lower by 20 to 30 °C than the case where no inside cooling is performed.

[0027] From the foregoing, the required flow rate of air is reviewed based on the heat balance between the air and the resin.

[0028] The heat quantity carried away by air from the system is as follows.

Specific heat of air	0.25 cal/g -°C
Air density	1.2×10^{-3} g/cm ³
Air temperature increase amount	25 °C
Mold inside cooling time	7 sec.
Air flow rate	F N1/min,

$$0.25 \text{ cal/g-}^{\circ}\text{C} \times 1.2 \times 10^{-3} \text{ g/cm}^3 \times F \text{ N1/min} \times 25 \text{ }^{\circ}\text{C} \times 1000 \text{ cm}^3/1 \times 7 \text{ s} \div 60 \text{ s/min} \quad \text{expression (1)}$$

[0029] On the other hand, the heat quantity taken away from the resin is as follows.

Specific heat of air	0.5 cal/g -°C
Weight of the bottle	W g
In case removing temperature of the bottle by inside cooling is lowered by 20 °C	

$$0.5 \text{ cal/g-}^{\circ}\text{C} \times W \text{ g} \times 20 \text{ }^{\circ}\text{C} \quad \text{expression (2)}$$

[0030] From the foregoing, because the expression (1) and the expression (2) is equal, the required flow rate of air is as follows.

$$F \cong 10 \times W \quad \text{expression (3)}$$

[0031] For example, in this case, since $W = 20 \text{ g}$, thus $F \cong 200 \text{ N1/min}$. In Fig. 5, if $F \cong 200 \text{ N1/min}$, it is known that the amount of temperature increase of air becomes constant and the ability of air per unit volume for taking away the heat from the resin becomes maximum.

[0032] In the conventional blow molding, the original pressure of the air was 4 to 7 kgf/cm² (G). Therefore, in case the inside cooling is performed, when the internal gas pressure of the bottle was set to 5 to 8 kgf/cm² (G), a sufficient inside cooling effect could not be obtained because the flow rate of air was too small.

[0033] On the other hand, when a large quantity of air was blown and discharged, the cooling effect from the mold was degraded because the pressure within the bottle was lowered.

[0034] When the original pressure of air of 4 to 7 kgf/cm² (G) was used conventionally, it was utterly impossible to flow such a large quantity of air as able to satisfy the expression (3) by setting the gas pressure within the bottle to 5 to 8 kgf/cm² (G).

[0035] Therefore, for example, by increasing the original pressure of air to 10 kgf/cm² (G), a large cooling effect can be obtained from both the inside and the outside of the bottle efficiently by flowing air of the flow rate satisfying the expression (3) when the pressure within the bottle is 5 to 8 kgf/cm² (G). Therefore, the removing temperature can be lowered.

[0036] In the present invention, the air having a room temperature of 20 °C is used. However, in case a cooled air is used, the removing temperature can be further lowered.

Brief Description of Drawings

[0037]

- 5 Fig. 1 is an air circuit diagram in an inside cooling device used for carrying out a blow molding process of the present invention;
 Fig.2 is a characteristic chart showing a relation between the removing temperature and the blowing pressure when no air is blown or discharged;
 Fig.3 is a characteristic chart showing a relation between the pressure within the bottle and the removing temperature at the body portion of the bottle when air is blown or discharged;
 10 Fig.4 is a characteristic chart showing a relation between the pressure within the bottle and the removing temperature at the bottom portion of the bottle when air is blown or discharged;
 Fig. 5 is a characteristic chart showing the relation between the air flow rate and the quantity of temperature increase of air; and
 15 Fig. 6 is a characteristic chart showing the relation between the cooling time and the removing temperature.

Best Mode for Carrying Out the Invention

[0038] One embodiment of a blow molding process of the present invention will be described hereinafter with reference to the drawings.

[0039] Fig. 1 is an air circuit diagram of an inside cooling device used for carrying out the blow molding process of this embodiment.

[0040] As shown in Fig. 1, the blow molding process of this embodiment is a blow molding process in which a gas is blown into a parison within a mold 7 to inflate the parison so that the parison is intimately contacted with a mold shaping portion to form a hollow molded product 6, and the gas is discharged from the interior of the hollow molded product 6 for the purpose of cooling.

[0041] The blow molding process of this embodiment is described in more detail.

[0042] An air circuit shown in Fig. 1 chiefly comprises a blowing side path for blowing gas such as air, or the like into a parison, and a discharging side path for discharging the gas blown into the parison. The blowing side path comprises a first blowing side path 14a, a second blowing side path 14b, and a third blowing side path 14c disposed over the entire distance between an air supply source 1 and a blow pin 5 hammered into a nozzle portion 8 of the mold 7.

[0043] A solenoid valve 3 is provided between the first blowing side path 14a and the second blowing side path 14b. A quick exhaust 4 for reducing the time for discharging air within the hollow molded product 6 and air within a piping is provided between the second blowing side path 14b and the third blowing side path 14c. A stop valve 2 for preventing entry of air is provided between the air supply source 1 and the solenoid valve 3.

[0044] The discharging side path comprises a discharge path 15 disposed over the entire distance between the blow pin 5 and a silencer 11. This discharge path 15 is provided at a location near the silencer 11 with a relief valve 10 for keeping pressure within the hollow molded product 6 in a prescribed range.

[0045] Pressure sensors 12 are provided each on an intermediate part of the third blowing side path 14c and on an intermediate part of the discharge path 15. Further, an air flow meter 13 is provided between the relief valve 10 and the silencer 11.

[0046] The blow molding is performed in the following manner, using the blow molding machine provided with the inside cooling device.

[0047] First, a sleeve-like molten resin called parison (not shown) extruded from an extruder is sandwiched between mold halves of the split mold 7, and then cut with a cutter (not shown). Thereafter, the blow pin 5 is hammered into the nozzle portion 8 of the mold 7. The mold 7 is provided with a plurality of cooling water circulating cavities 9 for circulating cold water.

[0048] Then, the solenoid valve 3 is opened and the air having an original pressure of 10 kgf/cm² (G) is blown into the parison from a distal end of the blow pin 5. As a consequence, the parison is inflated and urged against the mold shaping portion to form the hollow molded product 6. When the pressure within the hollow molded product 6 reaches a preset value of the relief valve 10, the air blown into the hollow molded product 6 is discharged from the silencer 11 by the relief valve 10 via the discharging side path 15. In this invention, the pressure of the relief valve 10 is set to 5 to 8 kgf/cm² (G).

[0049] About the pressure within the hollow molded product 6, the opening degree of a flow regulator such as a valve, or the like is regulated such that the pressure sensors 12 each provided on the first blowing side path 14a, the second blowing side path 14b, the third blowing side path 14c, or the discharging side path 15 indicate 5 to 8 kgf/cm² (G).

[0050] After the air is discharged for a prescribed time while blowing, the solenoid valve 3 is closed. When the pressure within the second blowing side path 14b is lowered, the quick exhaust 4 is actuated due to pressure difference

between the second blowing side path 14b and the third blowing side path 14c, and the air present in the third blowing side path 14c, the hollow molded product 6 and the discharging side path 15 is discharged.

[0051] After the pressure within the hollow molded product 6 is lowered to the atmospheric pressure, the blow pin 5 hammered into the nozzle portion 8 of the mold 7 is separated from the mold 7 and the mold 7 is opened for allowing the hollow molded product 6 to be removed therefrom.

[Example]

[0052] Next, a bottle was actually molded using the above inside cooling device. The molding conditions are as follows.

Bottle capacity	200 ml
Bottle weight	20g
resin	high density polyethylene (HDPE)
resin thickness	body portion: 0.5 to 1.5 mm, bottom portion: 1 to 3 mm
air blowing temperature	20 °C
mold cooling water temperature	17 °C

[0053] Fig. 6 shows results of the cooling time (blowing time + discharging time) and the removing temperature at the bottom portion in case no inside cooling is performed, in case the inside cooling is performed by setting the original air pressure to 5kgf/cm² (G), the pressure within the bottle to 4 kgf/cm² (G), the air flow rate to 100 N1/min, and in case the inside cooling is performed by setting the original pressure of air to 10 kgf/cm² (G), the pressure within the bottle to 6 kgf/cm² (G), and the air flow rate to 300 N1/min.

[0054] By this, in comparison with the case where no inside cooling is performed, in case the inside cooling is performed by setting the original pressure of air to 5 kgf/cm² (G), the pressure within the bottle to 4 kgf/cm² (G), and the air flow rate to 100 N1/min, the cooling time is shortened by about 15% (in case the removing temperature of 105 °C is served as a reference temperature, shortened from 7 sec. to 6.1 sec.). In case the inside cooling is performed by setting the original pressure of air to 10 kgf/cm² (G), the pressure within the bottle to 6 kgf/cm² (G), and the air flow rate to 300 N1/min, the cooling time is shortened proximately by 40% (shortened from 7 sec. to 4.4 sec).

[0055] As apparent from the test result, in the state where the gas pressure within the hollow molded product is 5 to 8 kgf/cm² (G), by discharging the air of the flow rate satisfying the above expression (3), i.e., in the above test, air flow rate of 200 N1/min or more, while blowing, the cooling effect from the mold can be maximized. Moreover, the cooling from the inside of the hollow molded product can also be performed efficiently and the cooling time can be shortened extensively.

[0056] The blow molding process of the present invention is not limited to the above embodiment but can be appropriately be changed without departing from the gist of the present invention. For example, in the above embodiment, the relief valve 10 is used as the pressure regulating valve. It should be noted, however, that by using a flow regulator such as a valve, or the like, the pressure within the hollow molded product 6 can likewise be regulated. In that case, the air blown into the parison is gradually discharged immediately after it is blown.

Industrial Applicability

[0057] As apparent from the hereinbefore description, according to the blow molding process of the present invention, the cooling effect from the mold can be maintained at its maximum level by maintaining the inside gas pressure of the hollow molded product to 5 to 8 kgf/cm² (G). In addition to this inside gas pressure, by discharging air of the flow rate satisfying the expression $F \geq 10 \times W$ [where F: gas flow rate (N1/min) and W: hollow molded product weight (g)] while blowing, a large cooling effect can be obtained from the inside of the hollow molded product.

[0058] Therefore, according to the present invention, a sufficient cooling effect can be derived by the mold from the outside of the hollow molded product and by air from the inside of the hollow molded product. Accordingly, a large cooling effect can be obtained without inefficiently using air. Thus, productivity can be enhanced by extensively shortening the cooling time.

Claims

1. In a blow molding process in which a gas is blown into a parison within a mold to inflate said parison so that said parison is intimately contacted with a mold shaping portion to form a hollow molded product, and the gas within said hollow molded product is discharged for the purpose of cooling,

said blow molding process being characterized in that an internal gas pressure of said hollow molded product is set to 5 to 8 kgf/cm² (G) and the gas satisfying the expression set forth below is discharged while blowing;

$$F \geq 10 \times W$$

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[where F: gas flow rate (Nl/min) and W: hollow molded product weight (g)]

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2. The blow molding process according to claim 1 wherein an air circuit of a device for cooling the interior of said hollow molded product comprises a blowing side path for blowing gas [such as air, or the like] into said parison, and a discharging side path for discharging the gas blown into said parison;

wherein said blowing side path comprises a first blowing side path (14a), a second blowing side path (14b), and a third blowing side path (14c) over the entire distance between an air supply source (1) and a blow pin (5) hammered into a nozzle portion (8) of said mold (7); and

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wherein said discharging side path comprises a discharge path (15) disposed over the entire distance between said blow pin (5) and a silencer (11), and said discharge path (15) is provided at a location near said silencer (11) with a relief valve (10) for keeping pressure within said hollow molded product (6) in a prescribed range.

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3. The blow molding process according to claim 2, wherein in said blowing side path, a solenoid valve (3) is provided between said first blowing side path (14a) and said second blowing side path (14b), a quick exhaust (4) for reducing the time for discharging air within said hollow molded product (6) and air within a piping is provided between said second blowing side path (14b) and said third blowing side path (14c), and a stop valve (2) for preventing entry of air is provided between said air supply source (1) and said solenoid valve (3).

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4. The blow molding process according to claim 3, wherein pressure sensors (12) are provided each on an intermediate part of said third blowing side path (14c) and on an intermediate part of said discharge path (15), and an air flow meter (13) is provided between said relief valve (10) and said silencer (11).

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Fig. 1

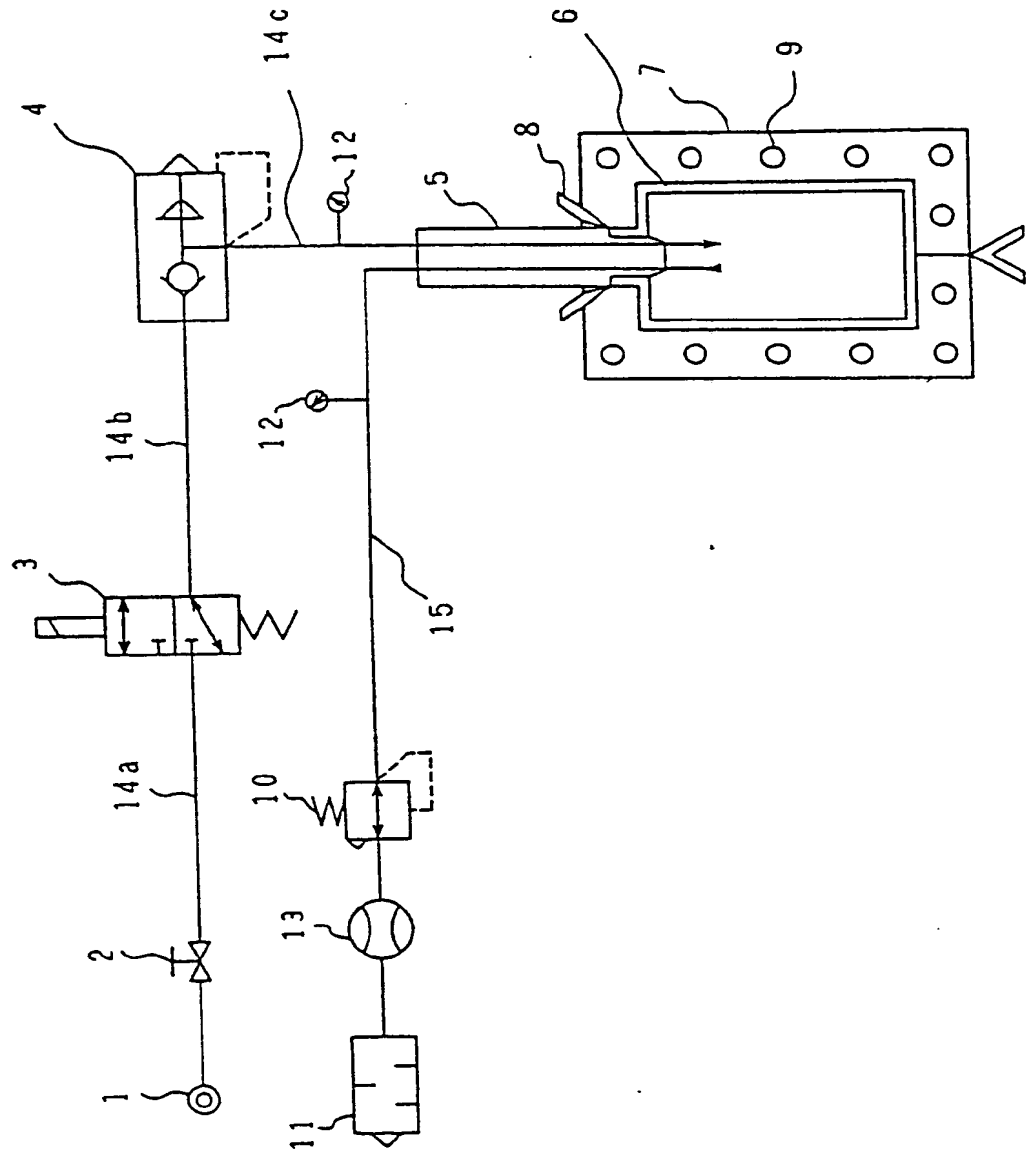


Fig. 2

RELATION BETWEEN REMOVING TEMPERATURE AND BLOW PRESSURE
AIR BLOWING/DISCHARGING, No

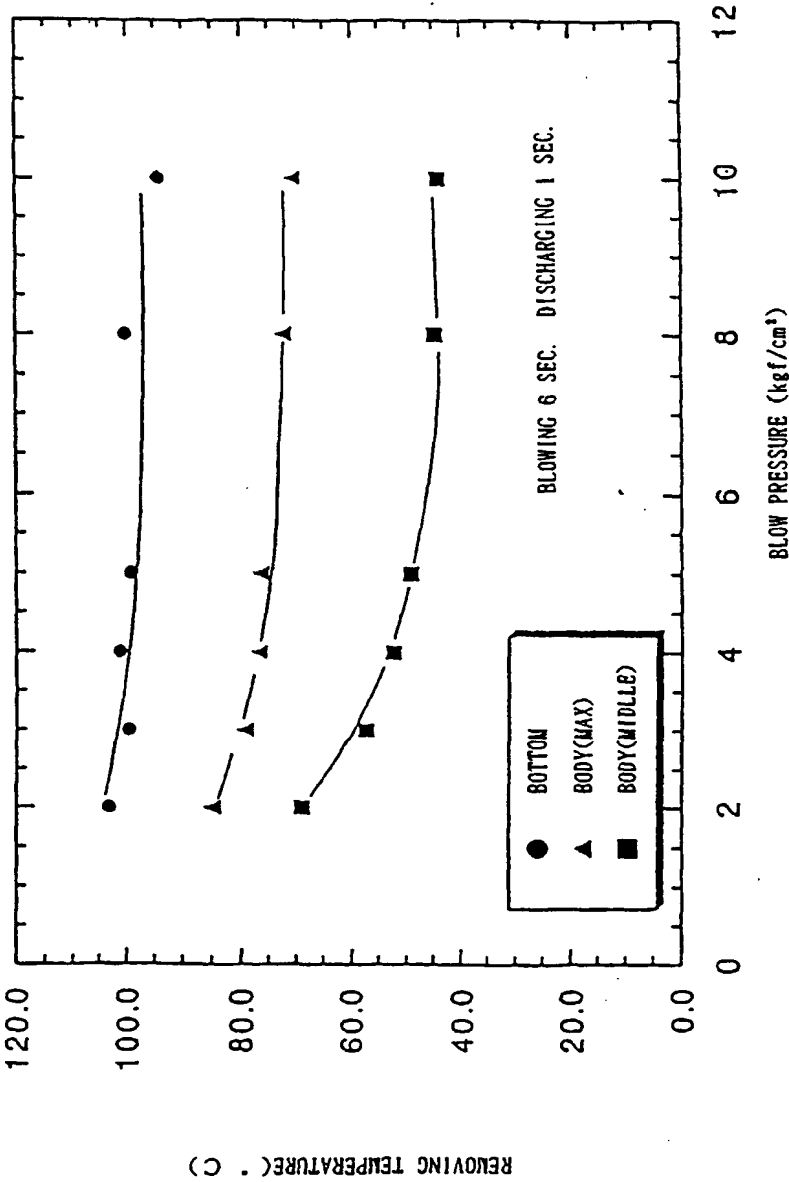


Fig. 3

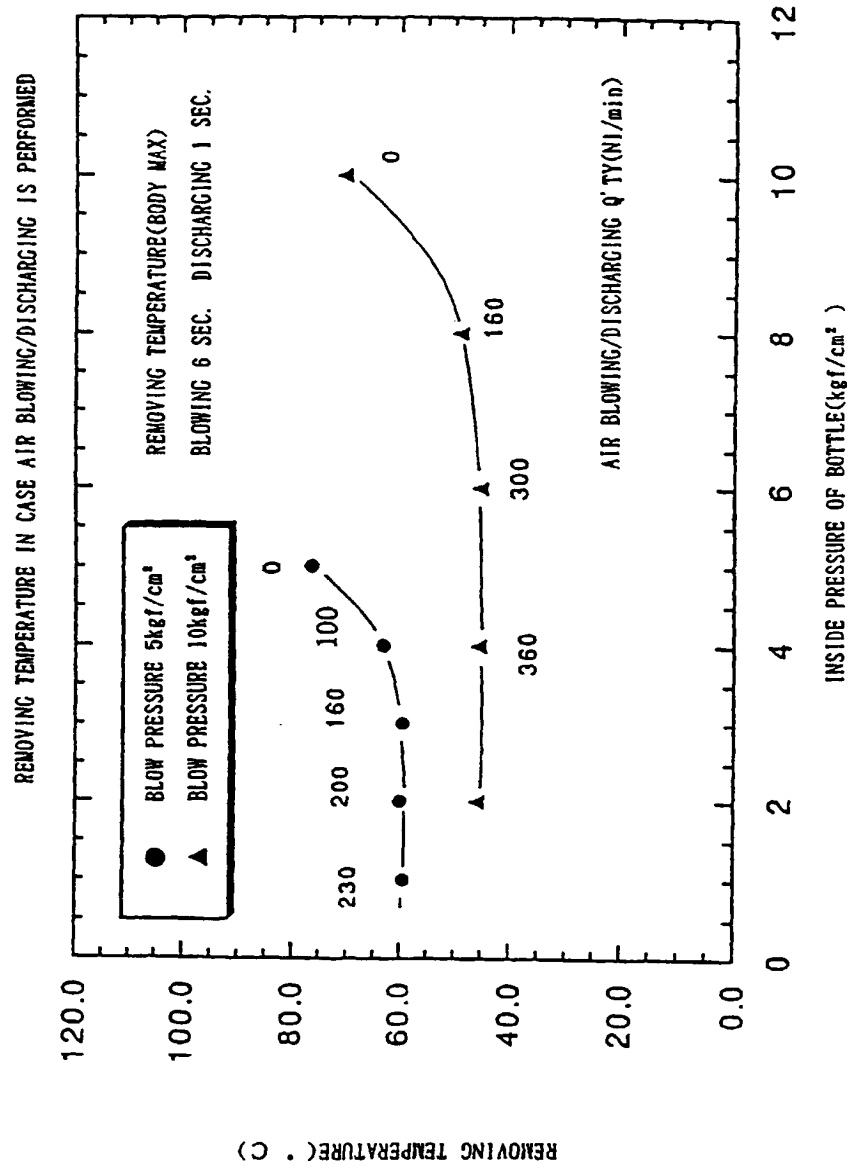


Fig. 4

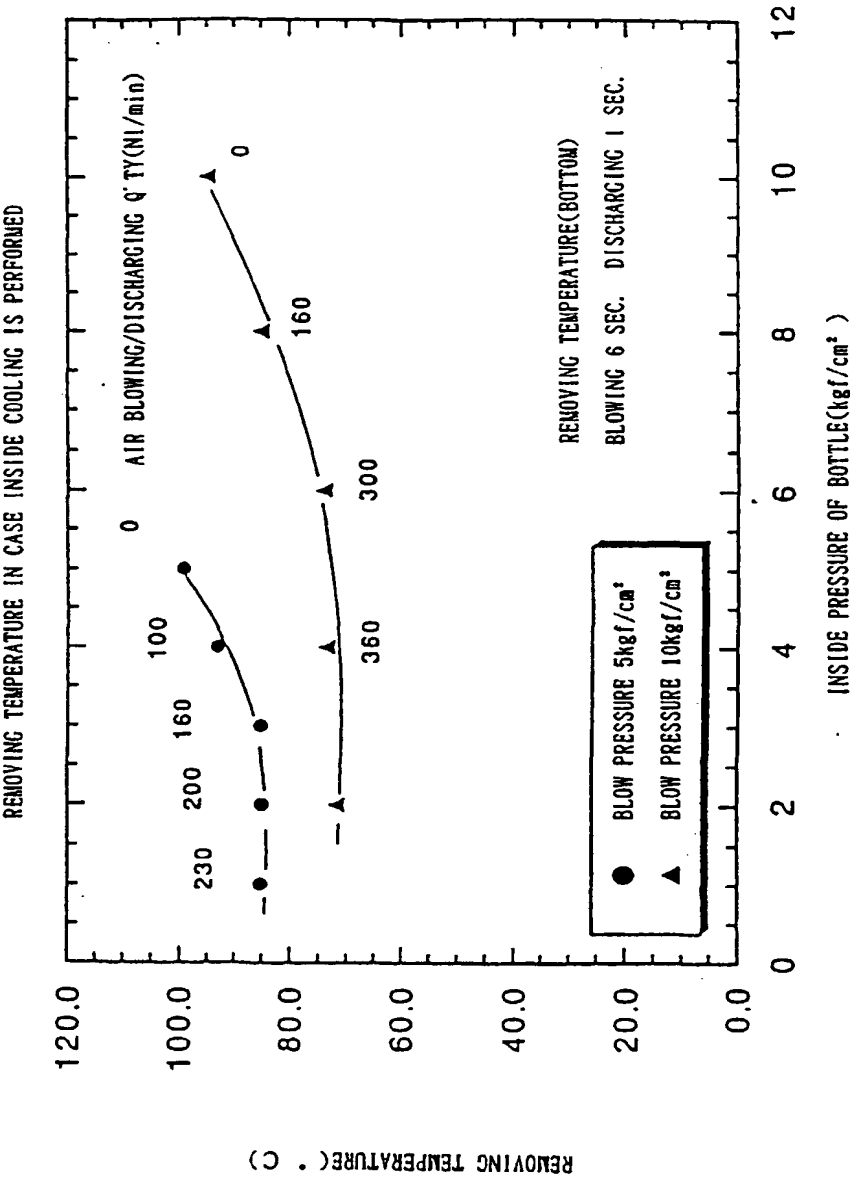


Fig. 5

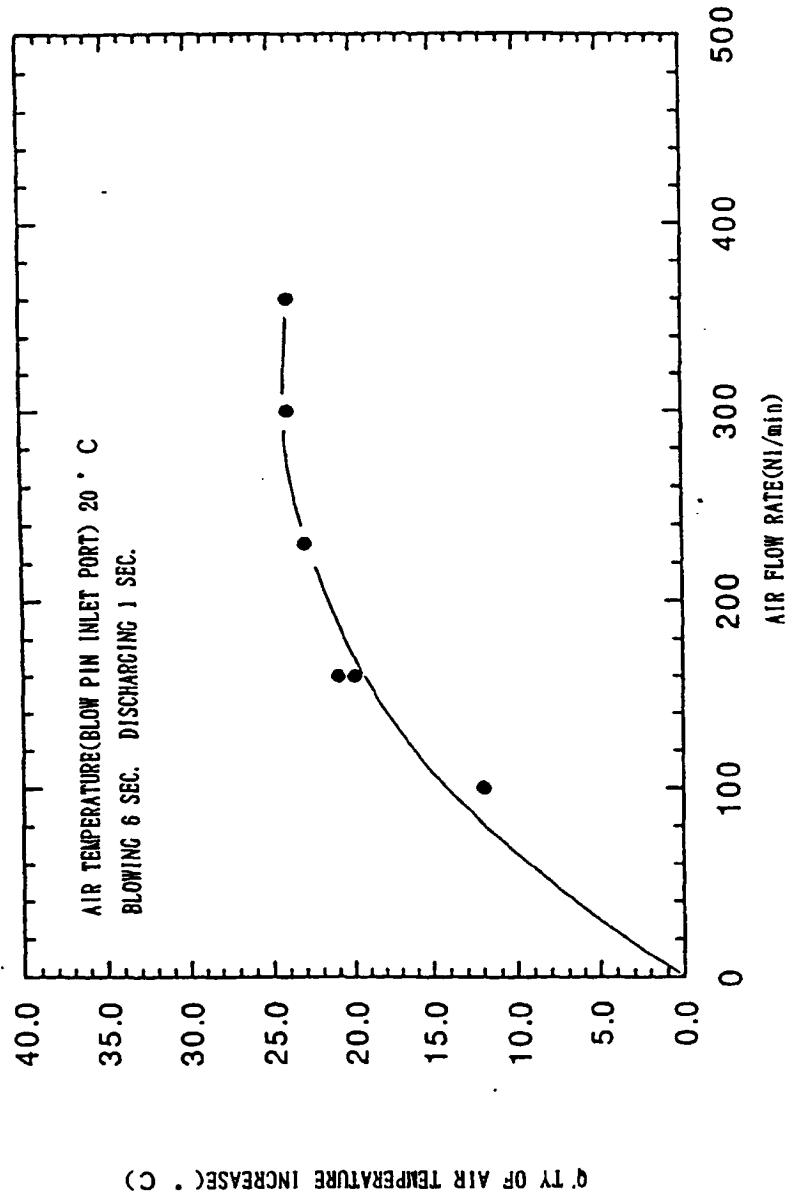
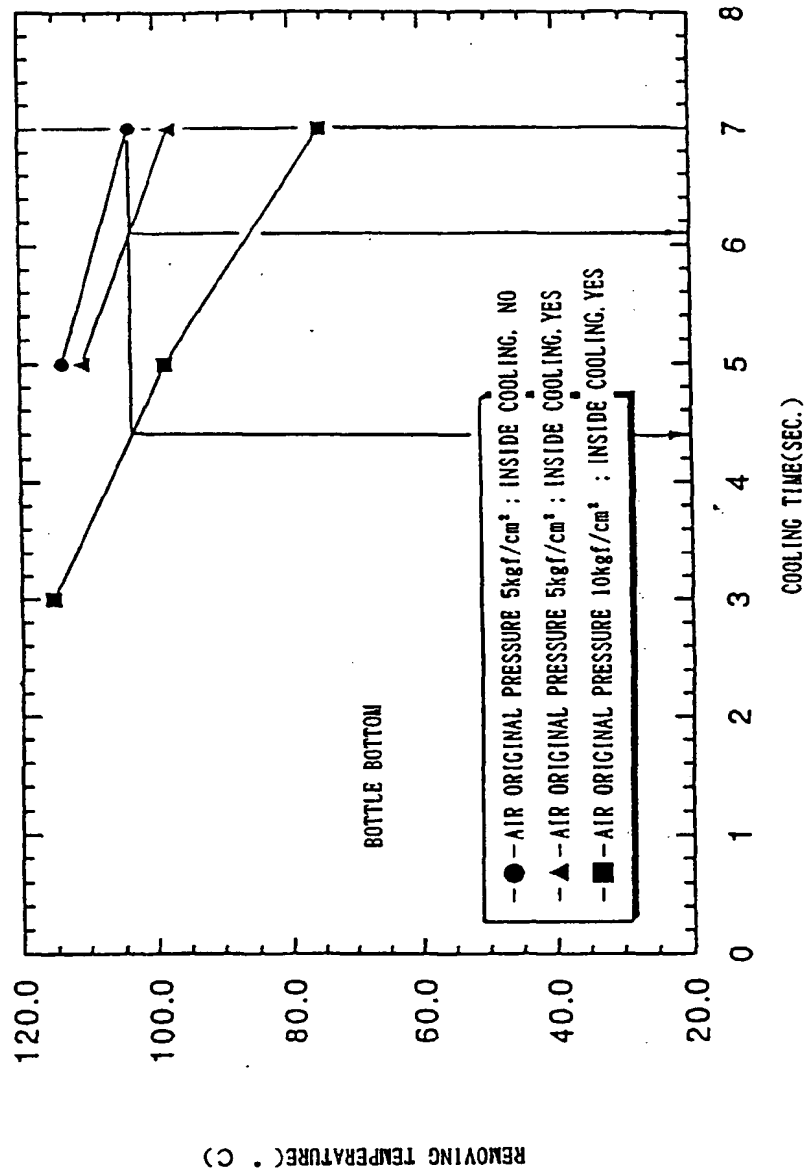


Fig. 6



INTERNATIONAL SEARCH REPORT

International application No.

PCT/JP97/00539

A. CLASSIFICATION OF SUBJECT MATTER

Int. Cl⁶ B29C49/66, B29C49/46, B29C49/78

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

Int. Cl⁶ B29C49/64-49/66, B29C49/46, B29C49/78

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Jitsuyo Shinan Koho	1926 - 1997
Kokai Jitsuyo Shinan Koho	1971 - 1997
Toroku Jitsuyo Shinan Koho	1994 - 1997

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	JP, 5-92476, A (Mitsubishi Plastics Industries Ltd.), April 16, 1993 (16. 04. 93) (Family: none)	1 - 4
A	JP, 3-274120, A (Honda Motor Co., Ltd.), December 5, 1991 (05. 12. 91) (Family: none)	1 - 4
A	JP, 3-9820, A (Asahi Chemical Industry Co., Ltd.), January 17, 1991 (17. 01. 91) (Family: none)	1 - 4

☐ Further documents are listed in the continuation of Box C.☐ See patent family annex.

* Special categories of cited documents:

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Date of the actual completion of the international search

May 9, 1997 (09. 05. 97)

Date of mailing of the international search report

May 20, 1997 (20. 05. 97)

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Form PCT/ISA/210 (second sheet) (July 1992)